

Design Feature

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Rectenna Serves 2.45-GHz Wireless Power Transmission

This fairly simple and straightforward rectenna design can be applied for conversion of energy at RF/microwave frequencies to usable DC power.

Wireless applications inject a great deal of excess electromagnetic (EM) energy into the environment—energy that can be reused if properly recovered. A rectifying antenna, or rectenna as it is popularly known, is one such means for recovering that energy. To demonstrate the capabilities of such a design, a novel rectenna was developed for low-power operation at a single Industrial-Scientific-Medical (ISM) frequency of 2.45 GHz.

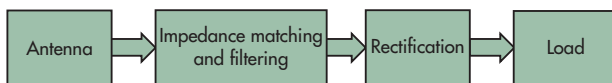
The rectenna consists of a highly efficient photonic-band-gap (PBG) structure, a microstrip lowpass filter (LPF) with

defected ground structure (DGS) circuitry, and a Schottky diode. To evaluate the rectenna, it was fabricated on a low-cost FR-4 printed-circuit-board (PCB) material with relative dielectric constant (ϵ_r) of 4.4 in the z-direction at 10 GHz and thickness of 1 mm. As will be shown, the rectenna achieves RF-to-DC conversion efficiency of 63% when processing received power of +18 dBm at 2.45 GHz.

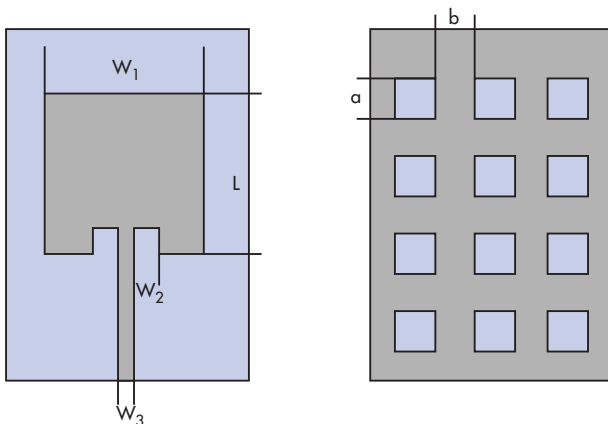
Studies of wireless transmissions, and methods for preserving and conserving the power from those transmissions, have continued since the first wireless power transmissions (WPTs) by Nikola Tesla in 1899. Rectennas have been of interest for their capabilities to convert RF energy to DC power, and provide the opportunities to “reuse” some of this transmitted wireless power. In recent years, microstrip circuit technology has been widely used for the development of receiving rectifier antennas, with RF-to-DC conversion efficiency representing one of the most important parameters of any rectenna design.¹⁻³

A rectenna is an antenna with additional components, including a LPF and a rectifying circuit. The rectenna receives microwave energy from the antenna.⁴⁻⁶ A Schottky rectifier diode converts the received RF energy to DC power.⁷⁻⁹ The amount of power that can be transmitted is limited, and the amount of RF/microwave power is reduced from the source through attenuation, mainly due to free-space signal path loss. For use in portable devices that, in general, usually have small dimensions, an effective rectenna design should also have small dimensions.

To achieve higher-order harmonic rejection of unwanted signals, the rectenna design employs a miniature microstrip LPF with DGS.^{10,11} The simple DGS is applicable on 50- Ω feeder lines to achieve the required lowpass filtering performance. The LPF with DGS can suppress and isolate second-



1. This diagram shows the main function blocks of the rectenna circuit.



2. This schematic diagram presents the linearly polarized PBG antenna for use at 2.45 GHz.

and third-order harmonic signals from the rectifying circuitry, allowing the rectenna to achieve its target high RF-to-DC conversion efficiency without processing unwanted signals.

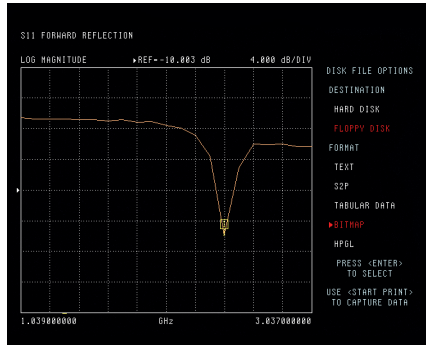
RECTENNA DESIGN

Figure 1 shows a block diagram of the proposed rectenna design. In developing this design, the PBG antenna, DGS LPF, and rectifier circuits were all first designed, fabricated, and characterized separately. Then they were combined to realize a complete rectenna.

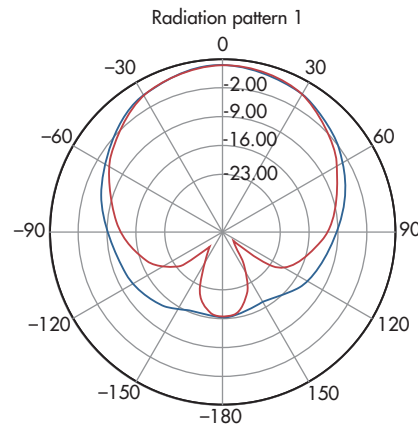
The linearly polarized PBG antenna was fabricated on 1-mm-thick FR-4 substrate with a relative dielectric constant of 4.4 at 10 GHz in the z-direction of the material (Fig. 2). The dimensions of the 50-Ω feed line were 20 × 1.9 mm. The dimensions of the PGB antenna were 30 × 31 mm. The photonic-band-gap (PBG) structure in the ground is designed to improve the gain as well as the directionality of the antenna. This increase in gain corresponds to improved power transmitting efficiency.

The square hole in the ground is designed for the PBG structure and it measures 6.6 × 7.0 mm. For some measure of the PGB antenna performance, Fig. 3 shows the antenna’s return loss while Fig. 4 offers its gain characteristics.

The rectenna’s DGS LPF was also designed and fabricated on FR-4 substrate material with relative dielectric constant of 4.4. With the U-slot added to it, the DGS offers good low-

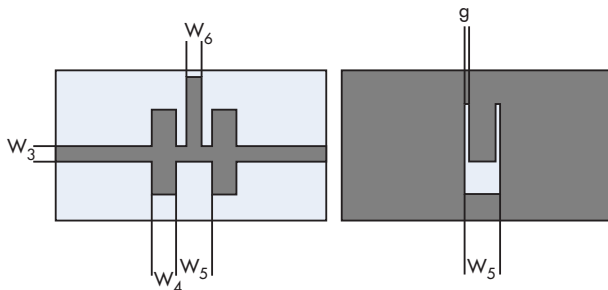


3. The plot offers measured results of return loss for the PBG antenna.



Name	Theta	Ang	Mag
m ₁	360.0000	-0.0000	3.6908
m ₂	180.0000	180.0000	-12.3883

4. These are computer-simulated results of the gain for the PBG antenna.



5. The schematic diagram represents the DGS LPF in the rectenna design.

pass characteristics with improved harmonic-suppression characteristics in the high-frequency stopband. The proposed DGS LPF exhibits sharp filter cutoff characteristics, with low in-band insertion loss, wide stopband, compact size, and relatively easy fabrication. The U-shaped slot is combined with a rectangular groove measuring 3.8 × 5.5 mm and a pair of gaps measuring 0.50 × 7.25 mm.

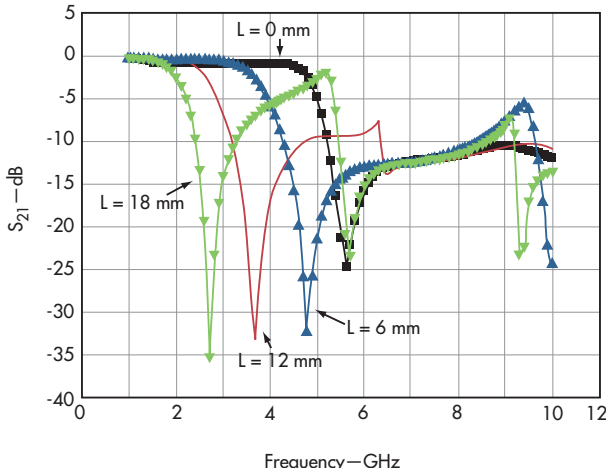
To achieve enhanced performance from the LPF, symmetric stubs were introduced to increase the filter’s band-stop suppression in the high-frequency band. Figure 5 presents the structure of the DGS LPF used in the rectenna. The optimal dimensions for the DGS LPF are as follows: W₄ = 3.6 mm; W₅ = 5.5 mm; W₆ = 1.5 mm; and g = 0.5 mm. For good bandstop characteristics, the length of the symmetric stubs can be of great importance.

As can be observed, the value of L greatly influences the band-notched frequency, as shown in Fig. 6. The bandstop frequency varies from 3.0 to 6.0 GHz as the value of L is varied from 0 to 18 mm.

In the rectenna design, the purpose of the rectifier is to directly convert RF/microwave energy into DC electrical energy. For this purpose, Schottky diodes are the preferred means of conversion for their low-voltage drops and high-speed response and processing capabilities. In addition, Schottky diodes consume the least amount of power due to conduction and switching of alternative RF-to-DC conversion approaches.

The commercial Schottky diode chosen for use in the rectenna design was model HSMS-286C from Avago Technologies (www.avagotech.com). This is a compact lead-free, surface-mount semiconductor that is usable from 915 MHz to 5.8 GHz. It features high detection sensitivity of as good as 50 mV/μW at 915 MHz, 35 mV/μW at 2.45 GHz, and 25 mV/μW at 5.8 GHz. The miniature surface-mount package helps save PCB space.

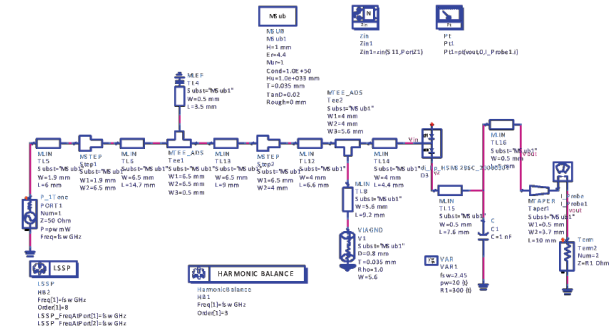
Within the rectifier circuit, the Schottky diode exhibits low parasitic circuit elements through about 6 GHz. High performance was achieved by modifying the basic parasitic circuit values and comparing them against the return-loss characteristics contained in the data sheet for the HSMS-



6. The curves show simulated values of S_{21} for different values of L .

286C. The main parameters for the HSMS-286C include series resistance, $R_s = 5 \Omega$; capacitance of $C_{j0} = 0.18 \text{ pF}$; and $V_{br} = 7 \text{ V}$. The next step was to create a matching input circuit for the diode, with matching done for the 2.45-GHz input. Figure 7 shows the simulated circuit module.

A matching circuit between the 50- Ω feed line and the RF-to-DC rectifying circuit is shown in Fig. 8(a). A peak efficiency of 63%, measured with a 250- Ω load, occurred at roughly +18 dBm received power, which is the maximum



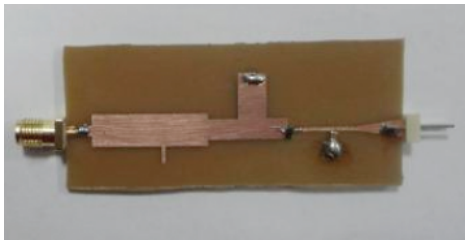
7. This schematic diagram represents the model used for the rectenna's impedance matching input circuit.

power rating of the diode. Loads of 200 and 300 Ω were also measured and produced nearly identical results. Figure 8(b) shows the conversion efficiency for the RF-to-DC rectifying circuit of these loads.

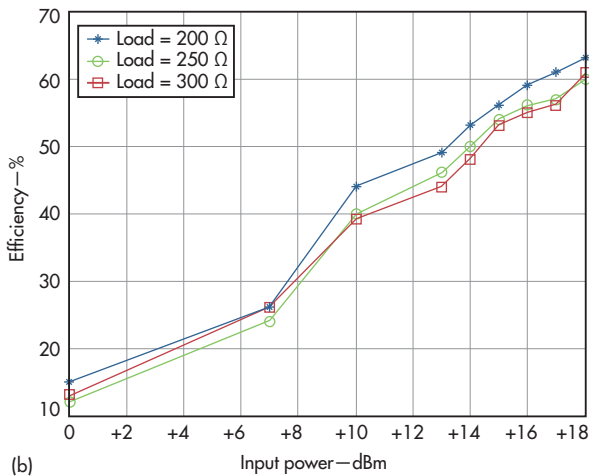
The rectenna shown in Fig. 9 was fabricated on a 1-mm-thick FR-4 substrate. It is designed to receive microwave energy in free space from a horn antenna with transmitted power levels to 4 W. The light-emitting diode (LED) is used as the low-power consumption load to verify the performance of the rectenna. Figures 10 and 11 offer glimpses of the test system used for this characterization. The rectenna was used to drive a single LED at a distance of 1 m and a voltage of +1.7 VDC.

The energy received by the rectenna was +7.3 dBm, which translates to an efficiency of 13.9%. The rectenna also drove an LED array formed by three LEDs at a distance of 75 cm and voltage of +1.8 VDC. The efficiency of the rectenna in this case can reach as high as 45.5%.

The rectenna with PBG antenna operating at the single ISM-band frequency of 2.45 GHz represents a fairly simple

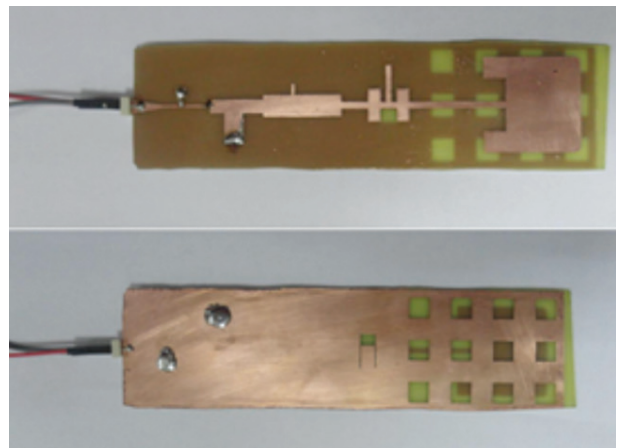


(a)



(b)

8. The proposed (a) matching circuit for the rectenna is shown next to its (b) measured electrical behavior



9. The proposed rectenna was fabricated on a 1-mm-thick FR-4 substrate.

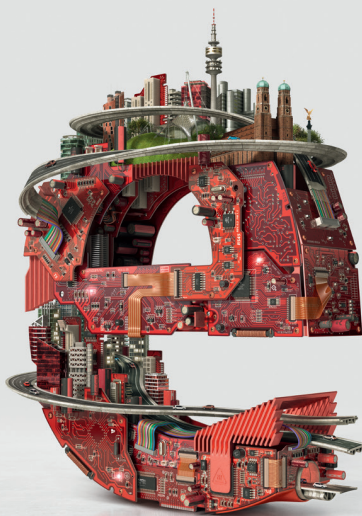
design and an effective means of converting RF signals to DC energy at that frequency. The gain of the rectenna is 4.29 dBi at 2.45 GHz, with RF-to-DC conversion efficiency of as high as 63%. This particular rectenna design can operate effectively with low-power loads at these ISM frequencies using a low-cost LED to aid in the conversion.

This rectenna design can contribute to low-power energy-harvesting applications at the ISM frequency band of 2.45 GHz. It was fabricated on relatively low-cost circuit substrate material with effective results, with the LED serving to assist in the operational stability while also indicating the proper operation of the rectenna circuitry. With its high gain and high RF-to-DC conversion efficiency, the rectenna represents a simple circuit addition for ISM-band products and an efficient means of reusing some of the energy that might otherwise have been lost. For compact and portable products, ideally the rectenna can be made with relatively small dimensions and at low cost.

This simple and straightforward conversion design can be applied to achieve power supplies for low-power loads, and can be useful in powering such applications as radio-frequency identification (RFID), wireless sensor networks, and micro-mechanical systems. **tmw**

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