By PETER MATTHEWS, Senior Technical Marketing Manager, and JARED BURDICK, RF Design Engineer, Knowles Precision Devices, [www.knowlescapacitors.com](http://www.knowlescapacitors.com)

# Keep Abreast of RF Filtering Trends (Part 2)

This closer of a two-part series covers the filtering solutions that can help RF filter designers stay on top of today's RF trends.

In the opener of our two-part RF filtering trends series, we discussed several emerging trends affecting the "jobs" RF filters need to perform. The article provides details on the overarching trend for mainstream applicati n [the opener](https://www.mwrf.com/technologies/components/article/21145154/keep-abreast-of-rf-filtering-trends-part-1) of our two-part RF filtering trends series, we discussed several emerging trends affecting the "jobs" RF filters need to perform. The article provides details on the overarching trend for mainstream applications to operate at increasingly high frequencies, resulting in the adoption of trends surrounding RF-filter performance considerations.

In part two, we take these ideas further by focusing on trends in today's filtering technology options and discussing filtering solutions that can help RF filter designers stay on top of those trends.

### **Higher Frequencies Drive a Shift**

As operating frequencies increase for many applications—which means the shrinking in size of many RF devices—there's an industry-wide trend to move away from using traditional lumped-element designs. In general, the lumped-element model doesn't work well at higher frequencies because it's difficult to manufacture the necessary discrete values without causing several other issues. Let's look at an example of a bandpass filter tee circuit centered at 28 GHz *(Fig. 1)*.

In this circuit, the series capacitance values need to be low, around 0.0094 pF, and shunt L values need to be around 0.027 nH, which are challenging to achieve with a lumped-element model. First, when using a wire-bond inductor, the coupling between each wire wrap will introduce a small amount of capacitance. The effect of this parasitic capacitance is magnified at higher frequencies, leading to self-resonance.

In addition, board-level parasitic effects result from mounting components and the transmission lines used in a lumped-element model. At high frequencies, these effects would essentially detune a filter. Thus, the small values needed in the example in *Figure 1* are difficult to produce because of the physical limits of manufacturing and tolerances noted here.

Therefore, at higher frequencies, RF engineers are shifting to a distributed-element model. As a result, transmission lines and waveguides are the primary methods for transferring electromagnetic waves around a circuit. Simply put, a transmission line is a two-conductor structure, and a waveguide is a single conductor with a hollow metal tube that provides distributed inductance with the empty space between providing distributed capacitance.

Furthermore, RF engineers can use different physical structures to move electromagnetic waves through a transmission line or waveguide. We can define the differences between the structures by looking at the modes each supports. In short, each mode describes a solution to Maxwell's equations with the boundary conditions for a given structure. That gives us the following three modes:

*Transverse magnetic (TM) mode*

The electric (E) field has components in the z-direction along the direction of propagation and the magnetic (H) field is transverse at right angles to the z-direction. Therefore, there's only an electric field along the direction of prop-



1. Shown is an example of an ideal, yet unrealistic, third-order response using a lumped-element model centered at 28 GHz.



2. Transverse-magnetic (TM) mode propagating in a rectangular waveguide. Looking at the waveguide along its length (red-shaded slice, 2.1), the E and H fields one would observe are as follows: In 2.2, the E field has components in the z-axis (there are components at right angles to the slice in 2.1) and in 2.3, the H field is transverse (there are components across the redshaded slice in 2.1) to the z-axis.



3. Transverse-electric (TE) mode propagating in a rectangular waveguide. Looking down from the top (red-shaded area labeled "A" in 3.1), one would find H fields (3.2) that have components parallel to the z-axis (circling around the plane of the red-shaded slice). Looking along the z-axis (blue-shaded area labeled "B" in 3.1), the observer will see E-field vectors (3.3) that are transverse (across the blue-shaded slide) to the z-axis.

agation *(Fig. 2)*.

*Transverse electric (TE) mode*

This has E-field components at right angles to the z-direction, meaning there's only a magnetic field along the direction of propagation *(Fig. 3)*.

*Transverse electromagnetic (TEM) mode* 

This has both E- and H-field components at right angles to the z-direction and no signals in the direction of propagation. Waveguides can't support TEM mode *(Fig. 4)*.

## **Comparing Filter Implementations**

The remainder of this article will look at trends affecting the different types of transmission lines and waveguide filters available today. But first, let's look at a more general "academic" view of the three main types of transmission lines used today and how the characteristics of these methods compare to the characteristics of a waveguide. The *table* shows, with all other qualities of the application being equal, how these methods compare, and *Figure 5* shows example drawings for each method.

While the *table* does highlight the traditional limitations of the different implementations, RF engineers are constantly innovating and pushing boundaries to work around some of these traditional constraints. Let's explore the emerging trends that are helping reduce or eliminate some of the traditional concerns with both waveguides and transmission lines.

# **Trends Impacting Waveguide-Based Filters**

Waveguide filters are, as the name



4. Transverse-electromagnetic (TEM) mode propagating in a coaxial transmission line. Looking along the length of the line (red-shaded cross section, 4.1), one would find that both the E-field vectors (4.2) and the H fields (4.3) are transverse to the z-axis.





suggests, filters constructed using waveguide technology. In general, the main advantages of a waveguide filter include high Q factor, which occurs as a result of using air as a dielectric, thanks to its high power capacity and near-zero loss. A primary disadvantage of waveguide filters, as illustrated in the *table*, is the relative size of these structures compared to filters that use a transmission line and can take advantage of TEM modes.

*Trend 1: Reducing waveguide filter size with ceramic dielectric resonators* 

To take advantage of some of the other qualities of waveguide filters, such as low loss and high Q, innovative RF filter designers are trying to address the size constraints of waveguide filters by changing the dielectric properties inside the cavity.

For example, one current size-reduction trend is to use ceramic dielectric resonators

R Round Wavequide Coaxial Line А C Rectangular Waveguide Microstrip and Stripline

 $\rm{with} \quad$   $\rm{a} \quad$   $\rm{high} \quad$   $\rm{dielectric} \quad$   $\rm{5.}$  Shown are the two types of waveguides and the three types of transmission lines noted in the table.



6. This image depicts a rectangular waveguide with dielectric resonators inside. 7. Here's a representation of a substrate-integrated waveguide (SIW).





constant inside an air-filled waveguide *(Fig. 6)*. Using ceramic instead of air reduces the wavelength of the radiation propagating through the material. This consumes less space, but it comes at a price because there will be higher loss when utilizing a solid dielectric instead of air.

*Trend 2: Reducing costs through 3D printing*

Another overall concern with waveguide filters is fabrication costs, which becomes a big issue when the end device is intended to be a high-volume, lowcost product. Costs are generally high

with waveguide filters because precision machining of metal cavities and ceramic components can be expensive and potentially cost-prohibitive in certain applications.

Likewise, one recent trend that may alleviate cost concerns in the future is the use of additive-manufacturing techniques such as 3D printing. Some prototypes have shown it's possible to employ 3D-printing techniques for components used at frequencies as high as the V band.

*Trend 3: Reducing size and costs with substrate-integrated waveguides*



8. Microstrips can be constructed with air as the upper substrate.

One new trend for developing waveguide filters that can address both size and fabrication cost concerns, which Knowles Precision Devices is digging into now, is the use of substrate-integrated waveguides (SIWs). An SIW is basically a rectangular waveguide in which the single conductor walls are formed by plated surfaces and vias, and in which TE mode is used *(Fig. 7)*. That means waves propagate in high dielectric-constant materials.

The key to developing an effective SIW is a thorough understanding of the materials needed to replace the air dielectric as well as the ability to precisely control the structures in a way that isn't cost-prohibitive. It's crucial to work

with a company that understands the highly engineered materials necessary to provide the right balance between the reduction in size offered by a high dielectric constant versus the potential for loss.

## **Trends Impacting Transmission-Line-Based Filters**

As mentioned, there are three main methods for developing transmission line-based filters: coax, microstrip, and stripline. Let's first look at transmissionline filter technology using ceramic coaxial TEM-mode resonators *(Fig. 4, again)*. These resonators can be combined with lumped-element components to create filter circuits. As a result, coax transmission lines tend to be used at lower operating frequencies, although this range is usually controlled by the physical dimensions of the resonator and the ceramic material's dielectric constant.

As noted in the *table*, the lingering concerns with this approach, which usually involves taking a series of ceramic coax resonators and stringing them together into a circuit, are the size constraints and the difficulty of integrating this type of filter into the wider circuit. However, it's important to note that relatively small ceramic coaxial resonators can be constructed as a result of continued innovation with material properties. This is still a largely mechanical approach to making filters, though, which may not be ideal because it can require additional "tuning" for the manufacturer.

In contrast to the coaxial approach, there's the relatively easy-to-use microstrip technology for building resonators and the associated circuit elements for filters. At a high level, microstrip is a type of planar transmission line that's simple to implement in printed circuit boards (PCBs). Composed of a strip conductor, dielectric substrate, and ground plate, microstrip is used in the microwave range with a typical maximum frequency of 110 GHz *(Fig. 8)*.

The main concern with using a microstrip approach, as shown in the *table*, is the loss experienced compared with other transmission-line and waveguide approaches. However, as noted, the industry is currently innovating on various materials to help address this constraint. The evolution of high-k materials, such as Knowles Precision Devices' PG, CF, and CG, are helping RF engineers develop low-loss mi-



9. These plots compare the loss per inch (a) and loss as the size of a wavelength changes (b) as frequency increases for Knowles Precision Devices' PG ceramic and RO4350 LoPro.

crostrip transmission-line filters.

*Figure 9* demonstrates how a microstrip transmissionline configuration using Knowles' PG ceramic reduces loss compared to RO4350 LoPro. Plot A illustrates loss/inch; plot B shows loss/wavelength. *Note:* We used the same material thickness, metal conductivity, and 50- $Ω$  microstrip transmission line in both configurations.

At frequencies above 13.6 GHz, PG material has better overall loss performance. This is largely because the surface roughness of PCBs is about four times greater than that of polished ceramics. Furthermore, as PCB materials are made thinner, the loss delta will become larger due to increasing surface roughness. Therefore, the frequency range in which polished ceramics outperform PCBs will grow. Combined with the benefits of loss/wavelength at higher frequencies, integrating passive RF components on polished ceramics is clearly the lower-loss option compared to PCB materials.

Finally, there's a stripline approach. Because stripline filters purely use TEM mode, there are clear benefits of stripline over microstrip. First, coupled-line structures don't need compensation for unequal phase velocities like those that can occur in microstrip. Also, there's less radiation using stripline. However, the Q, manufacturability, and tolerance all decrease with stripline versus microstrip, which means this method isn't as good of an option for applications that require higher Q and tighter tolerances.

### **Follow Trends for Effective Filters**

In general, while all RF applications need some level of filtering, there really isn't a one-size-fits-all RF filtering solution. Additionally, because applications that require RF filters are constantly pushing boundaries, the jobs RF filters can perform must evolve as well to keep up with today's cutting-edge technologies.

Therefore, it's imperative for RF engineers to keep pace with the latest trends affecting filter technology, such as those discussed in this two-part series, to ensure they have the most relevant information to develop the best possible filters for their applications. Often, this comes down to knowing the latest trends for materials, especially when it comes to selecting materials that will help address size and cost concerns, and precision manufacturing techniques that can ensure filters maintain high Q and tight tolerances.